

A Multi-element Microstrip Antenna for LTE Bands, Wi-Fi and WiMAX Application in Femtocell Network

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ABSTRACT

Interference management is the key point in the deployment of ultra-dense networks. Several techniques in physical and data-link layers have been discussed and proposed to provide lower power and better network capacity, while minimizing the cost and complexity of FemtoCell deployment. The applicability of an antenna with microstrip technology that employs multiple elements is developed here for coverage enhancement of FemtoCell network. The antenna proposed in this research has a size of $35 \times 35 \times 1.58 \text{ mm}^3$, it is printed on a commercially available FR4 dielectric substrate and designed for the frequency band from 1.9 GHz to 3.5 GHz. The different results obtained of the studied antenna in the FemtoCell scenario are discussed.

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1. INTRODUCTION

We believe that the densification of the network by using FemtoCells represent a commercially attractive solution to extend cellular coverage and enhance indoor network capacity in future 5G networks. FemtoCell is a miniature BS that operates in indoor environments and is envisioned to be useful for coverage enhancement and it would be an affordable solution to extend outdoor. It offers an excellent coverage in indoor areas and enhances the capability of the network by bypassing some of the data to a wired connection. A FemtoCell can be assimilated to a Small Office/Home Office (SOHO) network router that can be easy and simple to set up in offices and houses. Moreover, it is generally approved that increasing the number of cells with lesser radii will be a decisive factor in the next generation of cellular system (i.e. 5G) to increase the network capacity by providing required data rates [1]. These can be classified as "network densification", Issued by coverage densification and spectrum aggregation. Coverage densification is reached by improving multiple antennas at the FemtoCell Networks and extending the density of FemtoCell networks in a specified area. Recent research papers predict that small cells are the key technology to achieve 5G obligations [1], [2]. To meet the explosive growth of wireless data traffic and to satisfy the needs of 5G, where there is an anticipated 10,000 times more wireless data traffic and an increase in capacity by 2030 [3], original approaches and novel technologies are necessary. For that, antennas with multiple elements are seen as essential technologies in the emergence of the next generation of cellular wireless technologies (5G).

Antenna with multiple elements in FemtoCell scenario sectorizes spatially the coverage area into multi-sections and each of the elements takes the same portion of the desired region. 120° is assigned as the coverage angle for each of the three antenna elements, to maximize the spectral efficiency (SE) and to deal with the relentless demand for increased data rates [4], [5]. The planar microstrip patch antenna is widely used in the modern wireless communication systems for their attractive advantages, specifically mass-production facility, simple structural design, compact size, low profile, weight, constant gain, and stable radiation patterns [6]. Because of the attractive characteristics, microstrip line-fed antenna is widely used in appearing Small cell applications, and day by day research movement is increased focus on them.

In this paper, a patch antenna in microstrip technology is designed and fabricated for coverage enhancement of FemtoCell network with the use of multiple elements antennas (Figure 1). The development and analysis of the initial mode is computer-generated in a Three-element FemtoCell network like assembly. The design process outcomes, by making controllable beam directions in FemtoCell application. The continuity of this article is structured as follows: Antenna design in part two, results and discussion in part three, array arrangement in FemtoCell in part four and conclusion in part five.

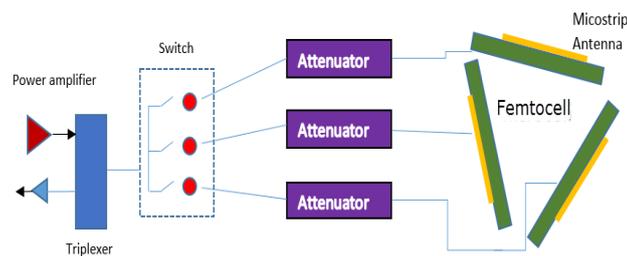


Figure 1. Multi-element antenna configuration in Femtocell (microstrip antenna)

2. ANTENNA DESIGN

The FemtoCell box has an enclosed area with limited space and accessibility for RF Circuits and antenna. Therefore, only specific types of antennas can be used for FemtoCell architecture. Actually, antennas with microstrip technology can fit with these requirements. As they are easy fabricated, lightweight and have low assembly cost. However, the process of designing a microstrip antenna is not always an easy task because the microstrip technology has many handicaps which must be taken into consideration in the preliminary phase of conception, for example, narrow bandwidth, small gain and low radiation pattern. Since the region of interest is indoor (about 1 to 10 m), multi-element antennas with microstrip technology for FemtoCell network is an attractive solution for the above type of application. Initially, the antennal structure was a simple monopole patch antenna, through a parametric optimization process by adding slots and trimming edges we got to the finale structure as shown in Figure 2. The antennas with microstrip technology are fabricated with various shapes and the most commonly designed antennas are: E, H, I, U, S slotted patch antennas [7-9], etc....

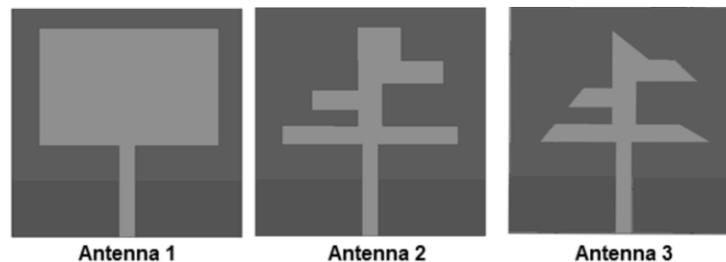


Figure 2. Evolution of the proposed antenna modeling

Here, the basic antenna was a classic rectangular patch that has undergone numerous changes in order to optimize the limitation of narrow bandwidth of a typical rectangular patch antenna by Bhatia [10] who specifies the width of the basic patch antenna as:

$$W = \frac{c}{2f_r \sqrt{\frac{\epsilon_r + 1}{2}}} \quad (1)$$

Where f_r and ϵ_r are frequency of operation and relative permittivity, one-to-one. Then, the effective permittivity is given approximately by Gilb [11] in this formula:

$$\epsilon_{\text{reff}} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left(1 + 12 \frac{h}{W}\right)^{-\frac{1}{2}} \quad (2)$$

Where h is the height or the thickness of the dielectric substrate used for the model of the studied antenna. [12] gives the real dimension of the microstrip patch length as:

$$L = \frac{c}{2f_r \sqrt{\epsilon_r}} - 2\Delta L \quad (3)$$

Where ΔL is the addition of the patch distance on the edges of the microstrip antenna that is set by Hammerstad [13] as:

$$\Delta L = 0.412h \frac{(\epsilon_{\text{reff}} + 0.3) \left(\frac{W}{h} + 0.264\right)}{(\epsilon_{\text{reff}} - 0.258) \left(\frac{W}{h} + 0.8\right)} \quad (4)$$

The ground plane dimensions can be considered as:

$$\begin{cases} L_g = 6h + L, \\ W_g = 6h + W \end{cases} \quad (5)$$

The Microstrip patch antenna in Figure 3 consists of three layers: ground, substrate and patch.

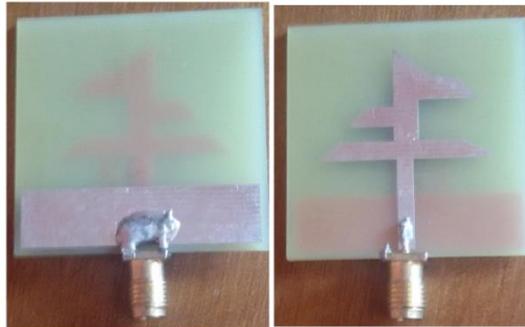


Figure 3. Image of the realized antenna

The dielectric substrate considered for the design of the proposed antenna is FR4_Epoxy with a thickness of 1.58 mm and a dielectric constant $\epsilon_r = 4.4$. It is generally known in the scientific committee that the use of substrates with a low thickness and dielectric constant makes it possible to reduce the size of the antennas [14]. It is widely known that the FR4 substrate is a lossy substrate and reveals poor performance with the increase in frequency. However, several research papers have successfully implanted the FR4 substrate in higher frequency bands (above 2 GHz) by miniaturizing the size of the antenna structure to reduce the effect of the substrate on the signal loss [15],[16]. The Antenna feed is performed by a microstrip line; this adapter is required to have 50Ω at the input of the microstrip antenna and to route the electromagnetics waves from the source to the antenna without causing reflections. The dimensions of the substrate are taken as $35 \times 35 \times 1.58 \text{ mm}^3$ and the size of the partial ground plane is $8.75 \times 35 \text{ mm}^2$. Figure 4 shows the top and bottom layers of the final geometry of the studied antenna. The optimal antenna parameters are summarized in Table 1.

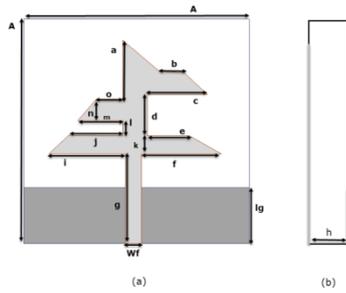


Figure 4. The geometry of the proposed antenna (not to scale),
(a) Top view, (b) Side view

Table 1. Optimal Parameters of the Proposed Antenna

Parameter	Value (mm)
A	35
h	1.58
a	9.4
b	3.8
c	9.3
e,d	6.5
f	12.4
g	14
i	11.9
j	8.3
k	2.8
l	2.4
m	7
n	3.1
o	4.3
wf	2.5
lg	8.75

3. RESULTS AND DISCUSSION

The S_{11} parameter versus frequency is shown in Figure 5. The first point is to estimate the effect of the ground plane on the widening of the bandwidth, a partial ground plane allowed us to expand the bandwidth, narrow with a full ground plane. The partial ground plane shows better return loss compared to the full ground plane.

VSWR and the S_{11} -Parameter can be used mutually to determine the matching of an antenna, The plot of VSWR against frequency shows that it is < 2 for the operational band of interest as shown in Figure 6. Figure 7 specifies the different values of the S_{11} -Parameter for our proposed antenna model. It was established that the antenna resonates in the desired frequency band as shown in Figure 6. Indeed, for $|S_{11}| < -10$ dB: the band ranges from 1.88 GHz to 3.6 GHz with two resonant frequencies at 2.4 GHz and 3.5 GHz. The bandwidth is approximately 1700 MHz which usually suitable for many LTE bands {1, 3, 7... 38, 40} broadly deployed in European, South American, Asian, and African countries [15, 16], Wi-Fi (2.4 GHz), and WiMAX technology (3.5 GHz) as described in Table 2.

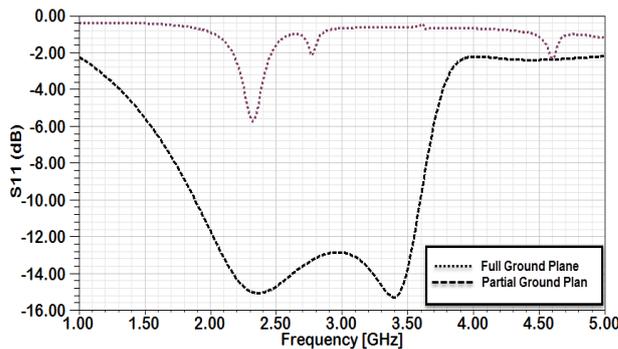


Figure 5. Comparison between the reflection coefficients S_{11} against frequency

Table 2. Current Major Spectrum Allocations for LTE, Wi-Fi and WiMAX Worldwide

Standard	Frequency Band (MHz)	World deployment
LTE Band 1	1920-2170	China, Japan, EU
LTE Band 2	1850-1990	North/South America
LTE Band 7	2500-2690	North/South America, Africa
LTE Band 33	1900-1920	-
LTE Band 34	2010-2025	China
LTE Band 35	1850-1910	-
LTE Band 36	1930-1990	-
LTE Band 37	1910-1930	-
LTE Band 38	2570-2620	EU
LTE Band 39	1880-1920	China
LTE Band 40	2300-2400	China, Asia
LTE Band 41	2496-2690	-
IEEE 802.11b/g/n (Wi-Fi)	2400-2500	Japan, EU, China, America.
WiMAX	2500, 3500	North/South America, EU, Africa, Asia, China

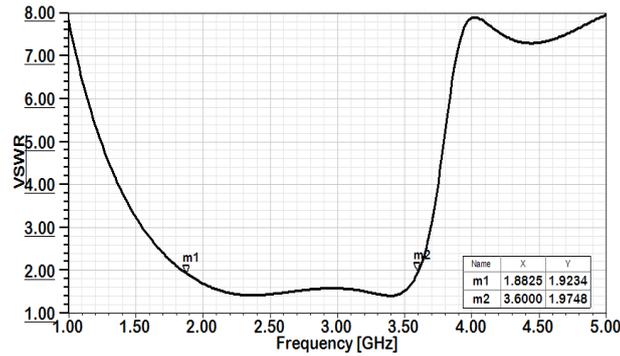


Figure 6: VSWR against frequency

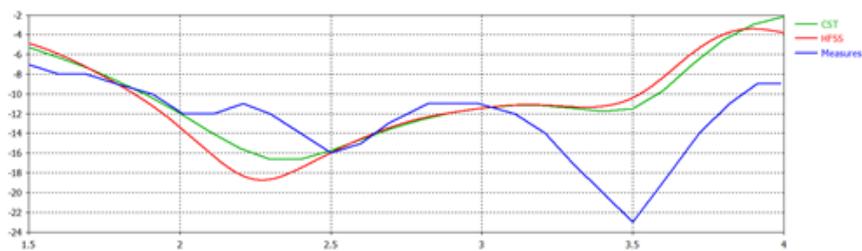


Figure 7: Reflection coefficients S_{11} against frequency

The main characteristics (Operational Bandwidth and Dimensions) of the proposed antenna are compared in Table 3 with some published work results in the literature.

Table 3. Results of All the References and Our Work

Article No.	Bandwidth (GHz)	Dimensions (mm ²)
Ref. [19]	1.93-3.74	60X50
Ref. [20]	1.93-3.6	55 X 15
This Work	1.9-3.6	35X35

Figures [8-9] shows the field pattern and the gain value of the proposed antenna at two frequencies 2.4GHz and 3.5 GHz. The E (x-y plane) and H (y-z plane) fields in the figures shows that they have almost good Omni-directional radiation patterns. It may be noted that the typical radiation patterns are dominated at both resonant frequencies: At 2.4 GHz (the inferior resonant frequency), the radiation pattern of the antenna is similar to that of a conventional monopole microstrip antenna in free space, with a so-called 'doughnut' shape. The radiation pattern at the higher functioning frequency becomes more irregular. For both cases, the shape of the partial ground plane affects the radiation patterns. The proposed antenna shows a very good Omni-directional radiation pattern even at lower and higher frequencies, which is required to receive data signals from all directions.

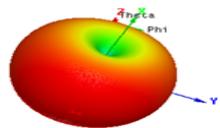
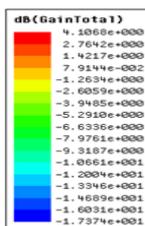


Figure 8: Simulated 3D Radiation pattern at 2.4 GHz

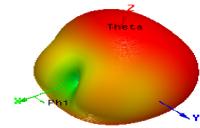
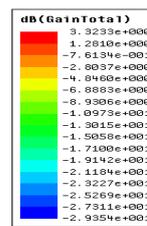


Figure 9: Simulated 3D Radiation pattern at 3.5 GHz

4. THREE-ELEMENT ANTENNA CONFIGURATION IN FEMTOCELL SCENARIO

Femtocell is mostly located in the corner of residential areas or offices where wired connection is available. Thus, in place of considering a conventional omni-directional antennas, a switched based multi-element structure is more suitable to enhance the coverage area. To estimate the applicability of this antenna in the FemtoCell scenario, three copies of the previously studied antenna are putted outside a pyramidal box. The three elements are oriented in three directions, placed on the three surfaces area of the pyramidal box as illustrated in Figure 10. Figure 11 illustrates different S parameters of the studied antenna. Since all three antennas are oriented with an angle of 120° to each other, the lateral lobes have no major impact on their radiation patterns.

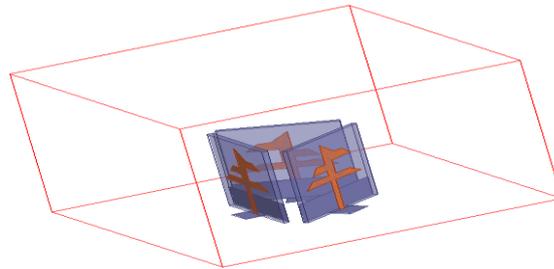


Figure 10. Concept of three-element antenna

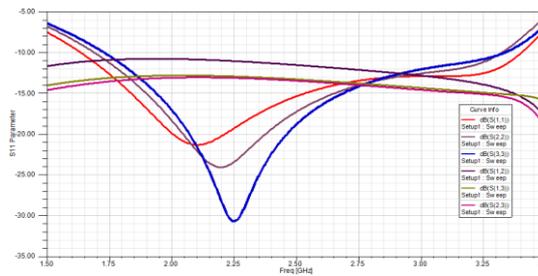


Figure 11. S parameters for multiple combinations of patch antennas

Figure 12 shows the Fairfield gain (Phi =0) of the Three-element antenna at the frequency 2.4 GHz. Thus, by modifying the power amplitude in excitation, the shape of the radiation pattern can be modified, and thereafter, meet the needs of a particular user by minimizing the interference between consumers and providing lower power and better network capacity.

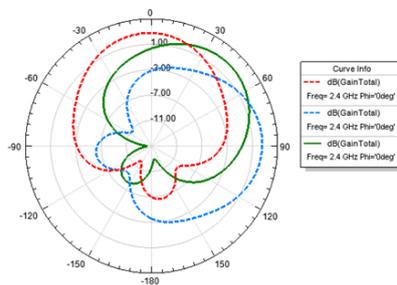


Figure 12. The Radiation Pattern of two microstrip antennas and their resultant beam at 2.4 GHz

5. CONCLUSION

In this paper, a simple, straightforward and most effective way to increase system capacity and provide coverage optimization by making cells smaller has been presented. The proposed FemtoCell microstrip antenna is simple to design and very compact with a size of $0.22 \lambda_{(f=1.9 \text{ GHz})} \times 0.22 \lambda_{(f=1.9 \text{ GHz})}$. It

provides good impedance matching from 1.9 GHz to 3.5 GHz. A low cost dielectric substrate FR4 substrate has been considered in the development of the studied antenna. Therefore, it can be deployed in large scale and with a great price–performance ratio

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